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Density and Strength
Of Gravel Concrete

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**DENSITY AND STRENGTH OF
GRAVEL CONCRETE**

BY

BENJAMIN PAYSON BURGESS

THESIS

FOR THE

DEGREE OF BACHELOR OF SCIENCE

IN

CIVIL ENGINEERING

COLLEGE OF ENGINEERING

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THIS IS TO CERTIFY THAT THE THESIS PREPARED UNDER MY SUPERVISION BY

BENJAMIN PAYSON BURGESS

ENTITLED DENSITY AND STRENGTH OF GRAVEL CONCRETE

IS APPROVED BY ME AS FULFILLING THIS PART OF THE REQUIREMENTS FOR THE

DEGREE OF Bachelor of Science in Civil Engineering

1001

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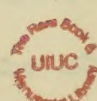
INTRODUCTION

The laws relating to the grading of sizes in concrete aggregate seem to have received very little attention at the beginning of the scientific study of this branch of engineering construction. Investigators set down only a few hard and fast rules that gave fairly good results, but did not give the best concrete attainable. Within recent years however some very careful and extensive tests have been made for determining the proportions of different sizes of the aggregate to use in order to obtain the densest and strongest concrete.

Two general methods have been used for determining the proportions in concrete; the first, to adjust the proportions so that the voids of the aggregate shall be filled with mortar and the voids of the sand with cement

INTRODUCTION

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paste; the second, to fix the proportions without any reference to the voids in the material. It has been found by experiment that a considerable saving of cement can be made by the use of more scientific methods of proportioning than those stated above. Though this reduction in the quantity of cement amounts to a considerable saving of cost in a large contract, the saving would not amount to much in a small job, and the usual methods would be more practicable.

The best known authentic and extensive tests on the proportioning of concrete were carried on at Little Falls, New Jersey, in 1901, and at Jerome Park Reservoir, New York in 1904, 05, and 06. The results of these experiments appeared in a paper by Fuller and Thompson before the American

Society of Civil Engineers in 1907. The general conclusion arrived at was, that the densest and strongest concrete was obtained when the mixture of the sizes of the aggregate gave for its mechanical analysis a curve that approached a parabola which had its beginning at the zero of co-ordinates and passed through the intersection of the curve of the coarsest stone with the 100 % line. Several important conclusions were drawn from these experiments.

(1) Aggregates in which particles have been specially graded in sizes so as to give, when water and cement were added, an artificial mixture of the greatest density, produce concrete of greater strength than mixtures of cement and natural materials in similar proportions. The

average improvement in strength by artificial grading under the conditions of the test was about 14%."

(2) "The strength and density of concrete is affected by the variations in the diameters of the particles of sand more than by the variations in the diameters of the stone particles."

(3) "The strength and density of concrete is affected slightly, if at all, by decreasing the quantity of the medium sized stones of the aggregate and increasing the quantity of the coarsest stones."

(4) "It follows from the foregoing conclusions that the correct proportioning of concrete for strength consists in finding, with any percentage of cement, a concrete mixture of maximum density, and increasing or decreasing the cement by substituting it

for fine particles of sand or vice versa."

(5) In ordinary proportioning with a given sand and gravel and a given percentage of cement, the densest and strongest mixture is attained when the volume of the mixture of sand and cement and water is so small as just to fill the voids of the larger particles. In other words, in practical construction, use as small a proportion of sand and as large a proportion of the larger particles as possible without producing visible voids in the concrete."

(6) The best mixture of cement and aggregate has a mechanical analysis curve resembling a parabola, which is a combination of a curve approaching an ellipse for the sand portions and a tangent straight line for the stone portion. The ellipse runs

to a diameter of one tenth of the diameter of the maximum size of stone, and the stone from this point is uniformly graded."

In the following pages will be stated the results and methods of a number of tests made by the writer. The methods and tables used in the experiments described by Fuller and Thompson before the American Society of Civil Engineers in 1907 were followed throughout so that a comparison of results could be made.

DESCRIPTION

General Method

Density and strength tests were made with gravel concrete using 10% of cement in all cases. Different combinations of sizes of sand and gravel were

used in order to study the effect of the grading of the sizes upon the density and strength of the concrete. The test for density was made by measuring the volume of concrete resulting from a definite weight of materials. For testing the compressive and transverse strength 6 inch cubes and 6"x6"x6'-6" beams were then made up from the concrete having the same composition of dry materials as used in the density tests.

Five different sets of tests were made, so planned that there should be a wide variation in the grading of the sizes. In four cases 2" stone was the maximum size used and in the fifth case the maximum size was $\frac{3}{4}$ " stone. In all cases the cement is included in the mixtures represented by

the mechanical analysis curves on Plate 3.

Mechanical Analysis

Mechanical analysis consists in separating the particles of any dry material used in concrete into a number of different sizes of which it is composed. The relative amounts of these separated sizes can then be represented by a curve the abscissae of which represent the diameters of the particles and the ordinates at any point the percentage of the total weight smaller than the corresponding diameter.

Cement

Chicago A A portland cement was used throughout the tests. Its strength, fineness, and specific gravity were tested and the results obtained are shown on Table 1.

TABLE 1.

Results of Cement Tests

| Fineness Test Parts in 1000 | | | Strength in Pounds per sq. in. | | | Remarks |
|--------------------------------|-----------------|--------------------|-----------------------------------|---------|--------|--|
| Sieve | Amt. Passing | Percent Passing | No. | Test 1. | Test 2 | |
| No. 200 | 802.00 | 80.2 | 1 | 805 | 720 | Sp. Gr. of Cement = 3.12 21.75% of water used. 7 day test |
| No. 150 | 969.00 | 96.9 | 2 | 730 | 650 | |
| No. 100 | 988.50 | 98.85 | 3 | 775 | 805 | |
| No. 74 | 1000.00 | 100.0 | 4 | 790 | 780 | |
| | | | 5 | 710 | 765 | |
| | | | Average | 762 | 744 | |

TABLE 2.

Sizes of Sieves

| Commercial Nos. of sieves in inches | Diameters passing sieves in inches | Commercial Nos. of sieves in inches | Diameters passing sieves in inches |
|---|--|---|--|
| 16 | .045 | 74 | .0071 |
| 20 | .034 | 100 | .0058 |
| 30 | .020 | 150 | .0036 |
| 40 | .016 | 200 | .0027 |
| 60 | .0115 | | |

TABLE 3

Specific Gravity of Gravel

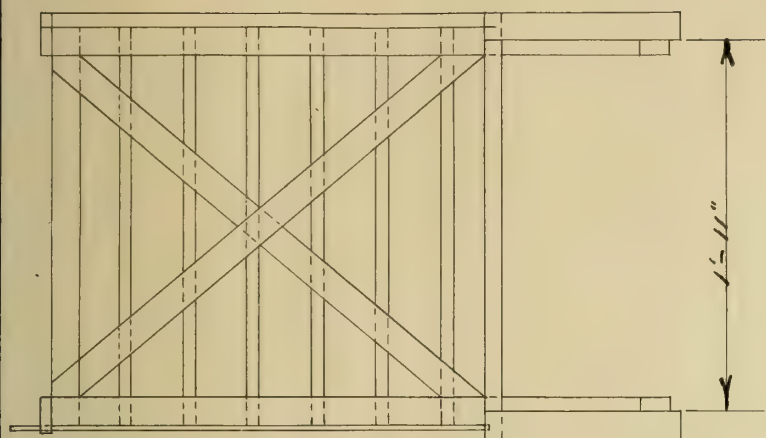
| Sizes | Average Sp. Gr. |
|--------------|--------------------|
| 2" - 1½" | 2.80 |
| 1½" - ¾" | 2.67 |
| ¾" - No. 16 | 2.63 |
| No. 16 - Pan | 2.61 |

Aggregate

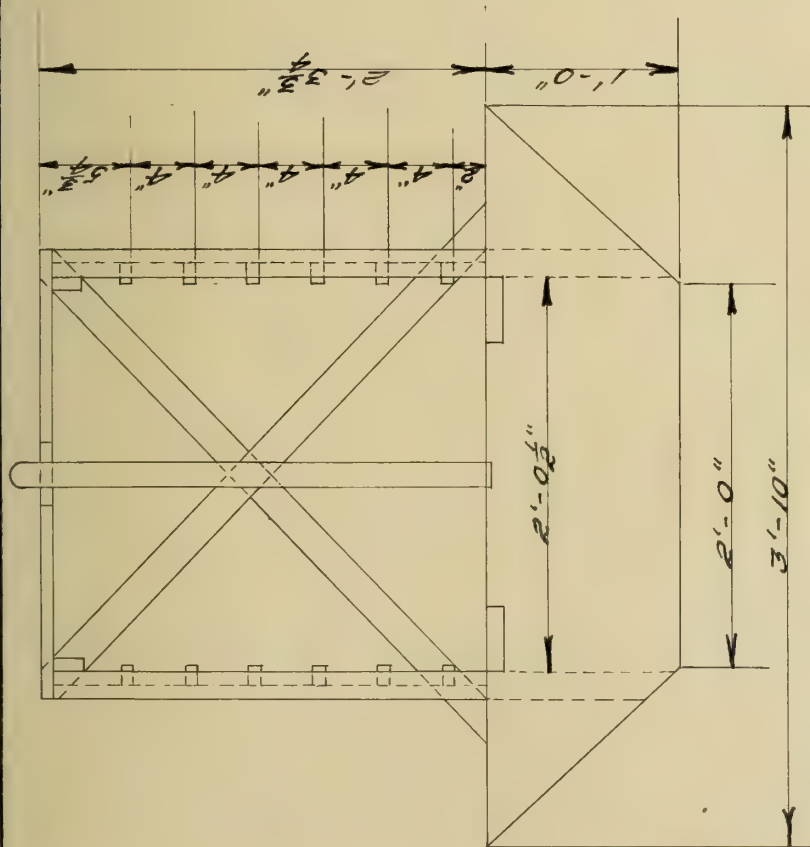
The aggregate used was fine washed gravel from along the Wabash river. Though it contained much foreign matter that usually accompanies commercial gravel, that part was removed as far as possible before the experiments were performed. Owing to the great lack of large sizes in the aggregate 2 inch and $1\frac{1}{2}$ inch sizes were obtained from other sources and these pieces were for the most part irregular pieces of granite.

Screening of Gravel

The gravel was separated into various sizes by means of square mesh screen and sieves. A rocking frame as shown in Plate 1 was built for screening the nine largest sizes. This frame was capable of holding five screens besides the tight box at the bottom. The gravel



END ELEVATION



FRONT ELEVATION

ROCKING FRAME

PLATE 1.

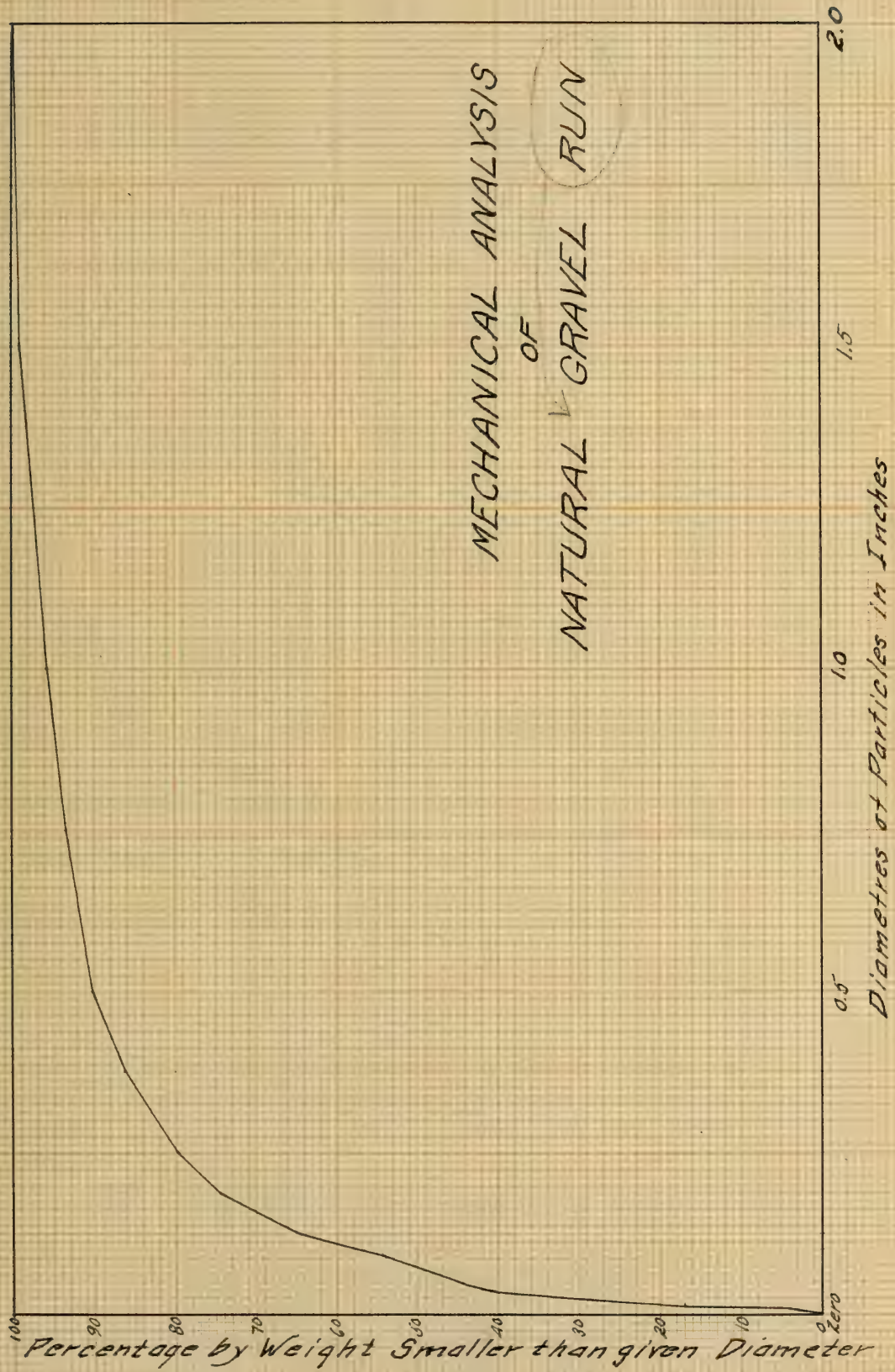
Scale 1 in = 1 ft.

was first shaken in the four largest screens for 2 minutes. The material going through all these screens and remaining in the box at the bottom was then shaken in the next five screens for 10 minutes. The part that then remained in the box was separated into the other ten sizes by means of a Howard and Morse Testing Sieve Agitator. This machine was run 30 minutes for each charge of $1\frac{1}{2}$ kilograms. A mechanical analysis of the natural gravel was made as described above and the results are shown in Table 2.

Specific Gravity of Gravel

On account of the great difference in the weight of the different sizes of the gravel a special method was devised to obtain the average specific gravity of the aggregate used in each mechanical

MECHANICAL ANALYSIS OF NATURAL GRAVEL RUN



analysis. An average was found for four different sets of sizes, the results of which are shown in Table 3, ^{p 9.}
 The amounts of these different sizes are obtained from the mechanical analysis table and by multiplying the amount by the different specific gravities and by dividing by the total amount the average for each curve was determined. The difference was found to be so small for the different curves that the average specific gravity of 2.65 was used for all cases.

CURVES

The curves are shown in Plate 3.

Curve No. 1. represents the average natural run of the gravel used.

Curve No. 2. starts at the vertical axis at 7% and runs as an ellipse to a point corresponding to 0.2 inch

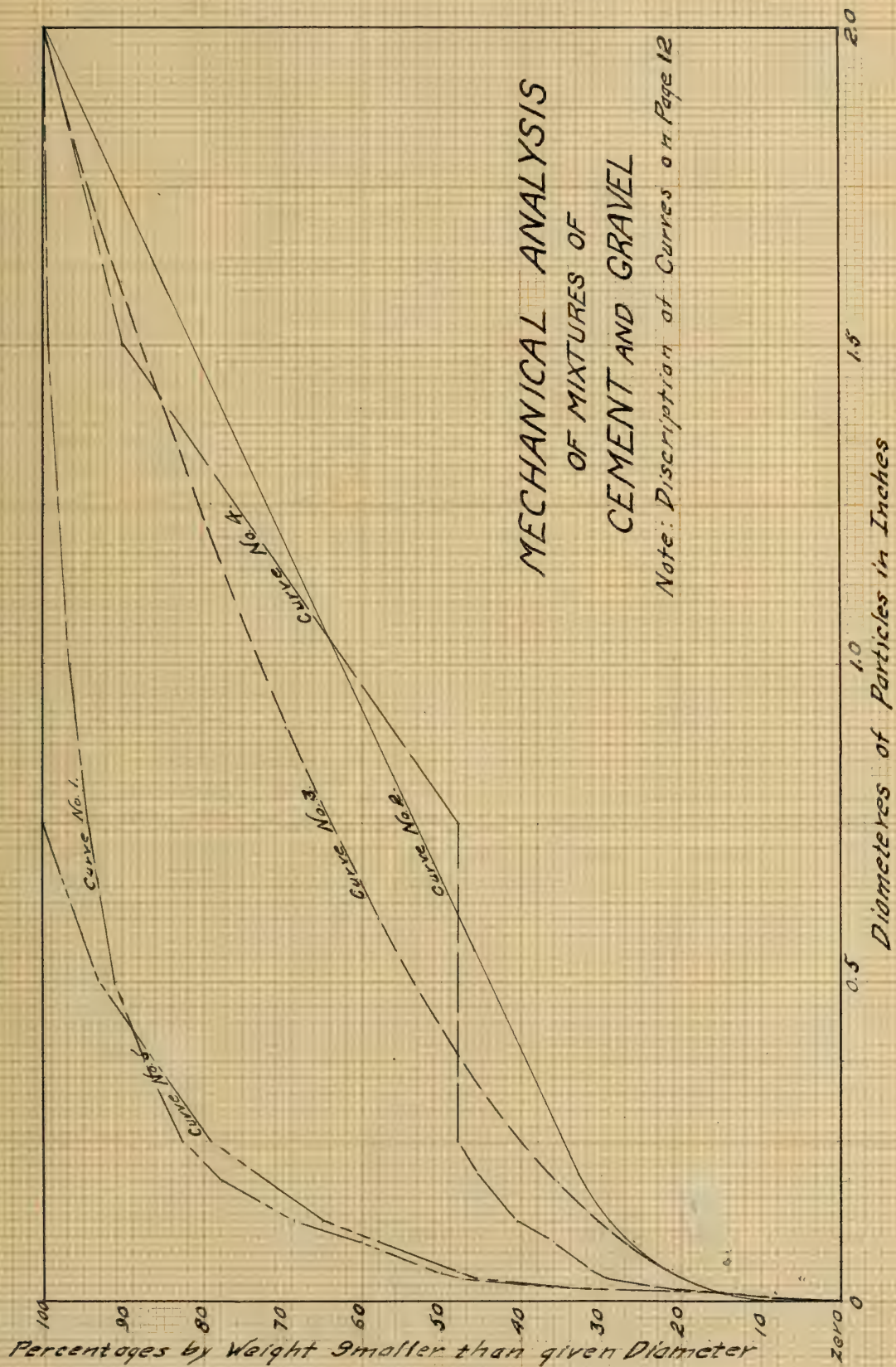


TABLE 4

Table of Percentages
of
Cement and Different Sizes of Aggregate
to
Total Weight of Dry Material

| Size of Particles in inches | Percents of Total Weight | | | | |
|-----------------------------------|--------------------------|------------|------------|------------|------------|
| | Curve No.1 | Curve No.2 | Curve No.3 | Curve No.4 | Curve No.5 |
| 2.00 - 1.50 | 0.80 | 18.70 | 12.40 | 10.00 | 0 |
| 1.50 - 1.00 | 2.80 | 18.70 | 14.90 | 28.00 | 0 |
| 1.00 - 0.75 | 2.10 | 9.35 | 8.70 | 14.00 | 0 |
| 0.75 - 0.50 | 3.20 | 9.35 | 10.60 | 0 | 7.00 |
| 0.50 - 0.375 | 3.60 | 4.68 | 6.10 | 0 | 7.00 |
| 0.375 - 0.250 | 5.80 | 4.68 | 7.43 | 0 | 7.00 |
| 0.250 - 0.1875 | 4.90 | 2.34 | 4.38 | 2.60 | 7.00 |
| 0.1875 - 0.125 | 9.10 | 3.33 | 5.23 | 4.80 | 7.00 |
| 0.125 - 0.09375 | 8.50 | 5.50 | 3.13 | 4.60 | 7.00 |
| 0.09375 - 0.045 | 10.20 | 2.36 | 6.19 | 5.40 | 10.00 |
| 0.045 - 0.034 | 2.80 | 1.72 | 1.82 | 1.40 | 2.60 |
| 0.034 - 0.020 | 11.20 | 2.78 | 2.81 | 6.00 | 11.20 |
| 0.020 - 0.016 | 9.80 | 1.01 | 0.98 | 5.10 | 9.40 |
| 0.016 - 0.0115 | 11.10 | 1.26 | 1.25 | 5.90 | 10.80 |
| 0.0115 - 0.0071 | 1.20 | 1.53 | 1.41 | 0.70 | 1.20 |
| 0.0071 - 0.0058 | 1.50 | 0.54 | 0.32 | 0.80 | 1.50 |
| 0.0058 - 0.0036 | 0.50 | 0 | 0 | 0.20 | 0.50 |
| 0.0036 - 0.0027 | 0.20 | 0 | 0 | 0.10 | 0.20 |
| 0.0027 - Pan | 0.70 | 2.52 | 2.40 | 0.40 | 0.60 |
| Cement | 10.00 | 10.00 | 10.00 | 10.00 | 10.00 |
| Total | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 |

size. From this point it is a straight line to the intersection of the ordinate 100% and abscissa 2.0 inch.

The equation of the ellipse was $(y-7)^2 = \frac{b^2}{a^2}(2ax - x^2)$ where $a = .36$ and $b = 29.0$. This equation and constants a and b were the same as for the "ideal curve" for gravel concrete in the Jerome Park tests, since the scope of the experiments here performed was not sufficient to permit preliminary tests to be made in order to find what ellipse would be the best for the gravel used.

Curve No. 3 starts at the vertical axis at 7% and runs as a parabola to the intersection of the ordinate 100% and abscissa 2.0 inch.

Curves No. 4 & 5 were broken line curves as shown on Plate 3 so chosen as to give new combinations of sizes of sand and gravel. In curve No. 5, $\frac{3}{4}$ " stone was the maximum

size used.

Density Tests

Weighing.

All materials were proportioned by dry weight, the gravel having been well dried over a steam drying apparatus before screening. In each test 20 kilograms of dry material were used. All weighing was done on Fairbanks Standard Scales. These scales weighed to the nearest 10 grams with a fair degree of accuracy.

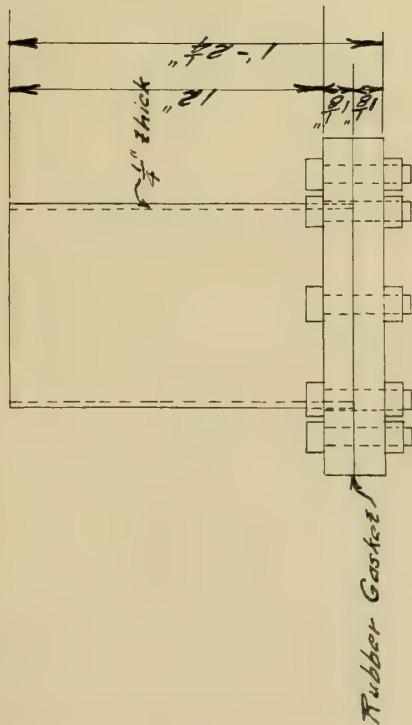
Measuring

The volume of the concrete was measured in an iron cylinder made of a short piece of wrought iron pipe as shown on Plate 2. The cylinder was carefully calibrated, but the results showed the line of calibration to be so near a straight line that the use of the curve was un-

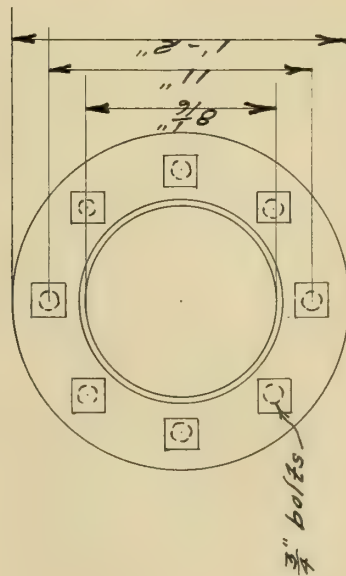
PLATE 2.

CYLINDER FOR DENSITY TEST

SCREEN FOR ROCKING FRAME

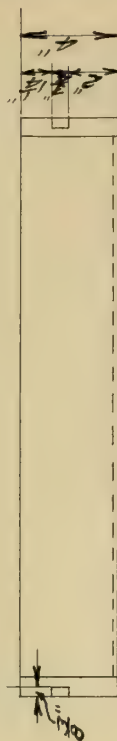


ELEVATION

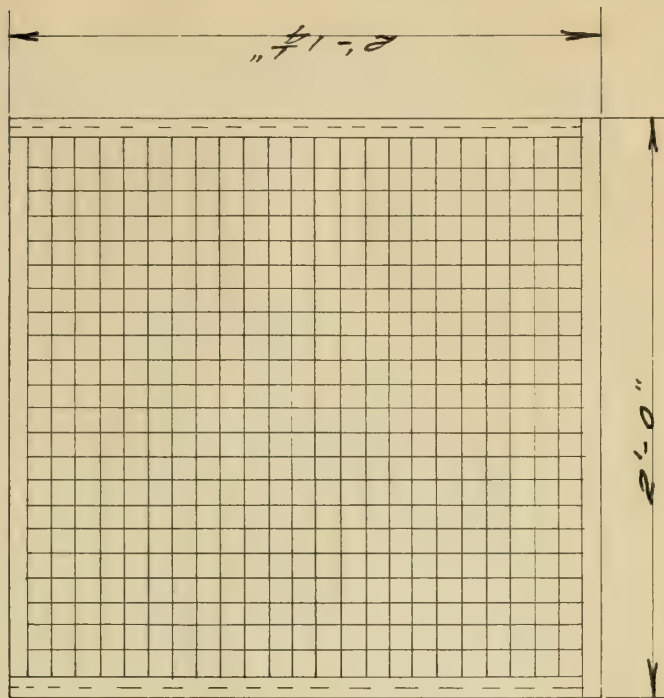


PLAN

FIGURE I.
Scale 1/32 in = 1 ft



ELEVATION



PLAN

FIGURE II.
Scale 1/32 in = 1 ft

necessary.

The materials were proportioned by the mechanical analysis curves. The mixing pan and all apparatus that might become coated with cement were weighed first. The aggregate, beginning with the larger sizes, was then weighed, the schedule of weights required having been so arranged that the different sizes could be put on top of one another in the pan, the poise being moved along the beam for each added quantity.

Mixing.

The cement and aggregate were first mixed dry until a uniform color was obtained. Water was then added in sufficient quantity so that after all was well mixed the mass was mushy and would hardly hold its form

in the pan. All mixing was done with a large trowel. The pail containing the water was weighed before and after the test and thus the amount used was determined.

Ramming.

The weight of the cylinder when empty having been previously determined the concrete was put in and well rammed with an iron rammer. If, after all the concrete was in the cylinder and the ramming completed, any surplus water remained on top, of the concrete this was removed by means of a syringe and the amount thus removed was weighed so that the water remaining in the concrete as set could be determined.

Final Weighing

The total weight of the cylinder containing the concrete and the weight of the tools having concrete sticking to them were weighed and the results recorded. The material sticking to the pan and tools was assumed to be for the most part cement and sand finer than .0071 of an inch in diameter; therefore this part was taken into consideration in figuring the density. The assumption was made that the fine sand and cement left sticking was in the same proportion as in the total mixture.

Measurement

After the surplus water was removed, the top of the concrete was smoothed off as much as possible and the distance from the top of the cylinder to the top

of the concrete was measured, by means of a steel rule, in several places around the circumference and an average taken. The total depth of the cylinder being known the depth of the concrete was easily computed. The data and results of the density tests are shown in Table 5.

Transverse & Compressive Strength Beams and Cubes

The concrete for the beams was made by the same general method that was used for the density tests. Wooden forms 6" x 6" x 6'-0" were used for the beams. These forms were made of 2" lumber and were not designed to keep the water from escaping from the bottom. They were held together by means of three clamps, one at each end and the third in the center.

TABLE 5.

*Density of Gravel Concrete
With Differently Graded Aggregates
Chicago AA Cement Wobash River Gravel*

| <i>No. of Curve</i> | <i>Percentage Cement to total Dry mix.</i> | <i>Max. size stone in inches</i> | <i>Calculated volume of material in one cubic foot of concrete as set in cubic feet</i> | | | | <i>Volume of Voids in 1 cu. ft.</i> |
|---------------------|--|--------------------------------------|---|------------------|------------------|--------------|---|
| | | | <i>Cement</i> | <i>Aggregate</i> | <i>Total Dry</i> | <i>Total</i> | |
| 1 | 10 | 2.0 | .065 | .686 | .751 | .989 | .249 |
| 2 | 10 | 2.0 | .073 | .775 | .858 | 1.020 | .142 |
| 3 | 10 | 2.0 | .077 | .812 | .889 | 1.051 | .112 |
| 4 | 10 | 2.0 | .072 | .775 | .847 | 1.020 | .153 |
| 5 | 10 | 0.75 | .066 | .700 | .766 | .974 | .234 |

Iron forms were used for the cubes. These forms were capable of holding three 6" cubes.

The mixed concrete was placed in the forms in 2 inch layers and rammed into place. Care was taken to trowel well along the sides of the forms so as to lessen the chance of large stones arching over and leaving voids along the sides.

Curing

The test specimens were left in the forms for seven days. At the end of that time, after the forms were removed, the cubes were buried in damp sand and the beams were left lying under cover, care being taken to wet them each day until they were tested at the age of 28 days.

Breaking

The cubes were broken by crushing in a Rickle two Screw Testing machine. The upper head of the machine was provided with a ball and socket joint. For three cubes no attempt was made to adjust the bearing surfaces; but in the others these surfaces were faced with plaster of Paris to equalize the pressure. Through a misunderstanding not all the cubes were broken under the same conditions.

The beams were tested in the same machine as the cubes, thirty and sixty inch spans with load applied at center being used. The two halves of the broken beam were used for the short spans. A 6" x 4" plank was used as a rest for the beam so as to cause a more gradual application of the load. The results of the beam and cube tests are shown in Tables 6 & 7.



TABLE 6

*Transverse Strength of Gravel Concrete
With Differently Graded
Aggregates*

| Reference No. | No. of equation Mech. Analysis Curve | Percentage Cement Dry Materials | Max. size stone in inches | Age in days | No. of Breaks | Transverse Strength in pounds per square inch | | | |
|---------------|--|------------------------------------|------------------------------|-------------|---------------|--|---------|---------------------|----------------------|
| | | | | | | Maximum | Minimum | Average for Beam | Average for Curve |
| 1 | 1 | 10 | 2.0 | 28 | 2 | 171 | 171 | 171 | |
| 2 | 1 | 10 | 2.0 | 28 | 3 | 194 | 179 | 186 | 178 |
| 3 | 2 | 10 | 2.0 | 28 | 3 | 407 | 267 | 316 | 316 |
| 4 | 3 | 10 | 2.0 | 28 | 2 | 354 | 344 | 349 | 349 |
| 5 | 4 | 10 | 2.0 | 28 | 1 | 408 | | 408 | |
| 6 | 4 | 10 | 2.0 | 28 | 3 | 390 | 294 | 345 | 361 |
| 7 | 5 | 10 | 0.75 | 30 | 1 | 113 | | 113 | |
| 8 | 5 | 10 | 0.75 | 30 | 2 | 127 | 83.5 | 115 | 114 |

TABLE 7

*Compressive Strength of Gravel Concrete
With Differently Graded Aggregates*

| Reference No. | No. of equation of Modul. Analysis Curve | Percentage Cement Dry Materials | Max. size stone in inches | Age in days | Compressive Strength in pounds per square inch | | Bearing Surface |
|---------------|--|------------------------------------|------------------------------|-------------|--|----------------------|-----------------|
| | | | | | Maximum Single Cube | Average for curve | |
| 1 | 1 | 10 | 2.0 | 28 | 768 | | Plain |
| 2 | 1 | 10 | 2.0 | 28 | 756 | 762 | " |
| 3 | 2 | 10 | 2.0 | 28 | 2160 | | Plaster Paris |
| 4 | 2 | 10 | 2.0 | 28 | 2260 | 2210 | " " |
| 5 | 3 | 10 | 2.0 | 28 | 2834 | | Plain |
| 6 | 3 | 10 | 2.0 | 28 | 2660 | | Plaster Paris |
| 7 | 3 | 10 | 2.0 | 28 | 2850 | 2781 | " " |
| 8 | 4 | 10 | 2.0 | 28 | 2120 | | " " |
| 9 | 4 | 10 | 2.0 | 28 | 2300 | 2210 | " " |
| 10 | 5 | 10 | 0.75 | 28 | 410 | | " " |
| 11 | 5 | 10 | 0.75 | 28 | 480 | 445 | " " |

CONCLUSION

The following conclusions, drawn by Fuller and Thompson, as quoted in the first part of this article, were verified by the results obtained:-

(1) That the densest concrete is the strongest.

(2) That the substitution of coarser stone for medium sized stone had little effect, if any, on the density and strength.

(3) That a large amount of sand greatly reduced the strength and density.

The ellipse and tangent curve did not appear to be the ideal one for the materials used from the results obtained since the parabola gave denser and stronger concrete. The conclusion drawn from this is that more fine material was necessary to give the ideal curve for the

gravel used than this ellipse curve gave. This conclusion is not definitely proved since so few tests were made and the amount of error that was apt to come in on account of the inexperience of the performer made positive proof impossible.

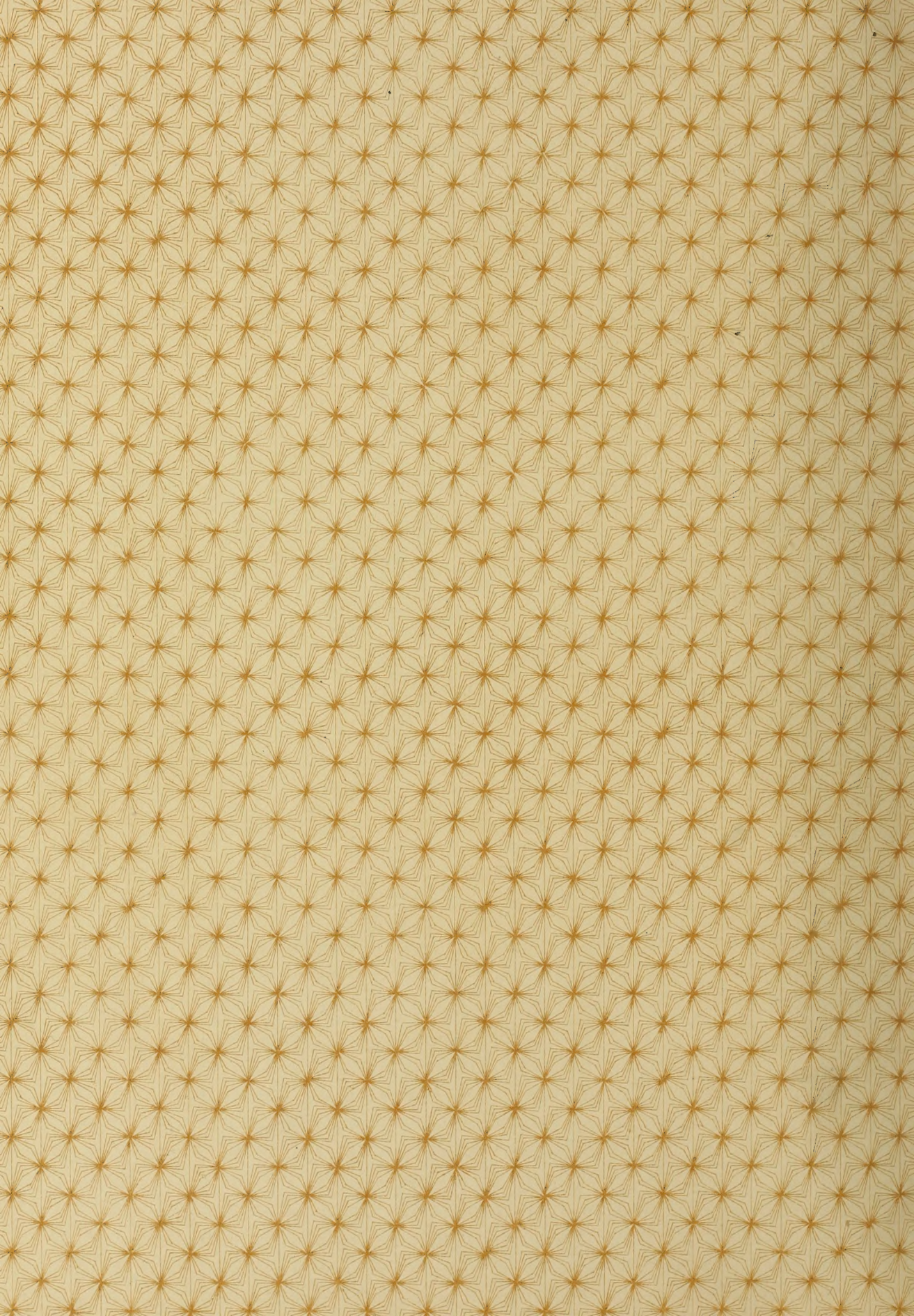
In a continuation of this work it would be advisable to use cubes altogether instead of cubes and beams. The reason for this is that cubes being smaller a great many more could be made with the material used in the beams and although the breaking results might be a little more variable because a difference of bearing surfaces gives large variations the greater number would more than offset this objection. A 6 inch cube is not large enough to make a test for concrete with stone

2 inches in diameter because with a small sized cube there is too much chance for the stones to arch and leave voids.

On account of the great comparative amount of the size that would go through a No. 200 sieve that was needed, the time and money spent in sifting this size material was excessive. This difficulty could be easily removed by using 12% of cement instead of 10% because the cement could be substituted for the small sizes in the sand.

On account of the small capacity of the apparatus used for sifting out the small sizes of aggregate a great deal of time was needed to obtain the amount of these sizes necessary. About 42 hours of continual sifting is taken to obtain 1 kilogram of the size

that goes through a No. 200 sieve.
For this reason it is seen that in
order to get the work completed
as expeditiously as possible the
material ought to be sifted a
long time before the tests are
to be made.





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